Classic Bearing Damage Modes

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Goals

- Introduce to classic bearing damage modes
 - Recognize types of bearing damage
 - Offer possible causes for bearing damage
 - Suggestions for the prevention of damage
- "White Etch Areas" damage mode
 - Terminology
 - Background on microstructural alterations
 - Recent transmission electron microscopy (TEM) investigations



How is bearing life defined?

- A rolling mill roll neck bearing may have extended service life even with signs of damage if properly repaired.
- High speed dental hand piece bearing life determined by bit speed at a given driving pneumatic pressure.
- Wheel end bearing for mining truck may be limited by peeling and spalling damage.
- Medical equipment bearing life limited by noise and vibration characteristics.
- Wind turbine main shaft bearing limited by occurrence of spalls.

Divide damage modes into two categories:

Material Fatigue & Wear



Bearing Damage Modes:

Material Fatigue

- L₁₀ fatigue life the number of hours (or cycles) that 90% of a group of (apparently identical) bearings will meet or exceed, under a given set of conditions, before specified fatigue damage occurs.
- Life models predict statistical likelihood that material defects in cyclic stressed volume will create spalls.
 - Factor-based analysis (catalog with adjustment factors)
 - Stress-based analysis
- Adjustment factors on predicted life account for:
 - Reliability
 - Material
 - Environmental conditions (lubrication, misalignment, debris...)

Where You Turn

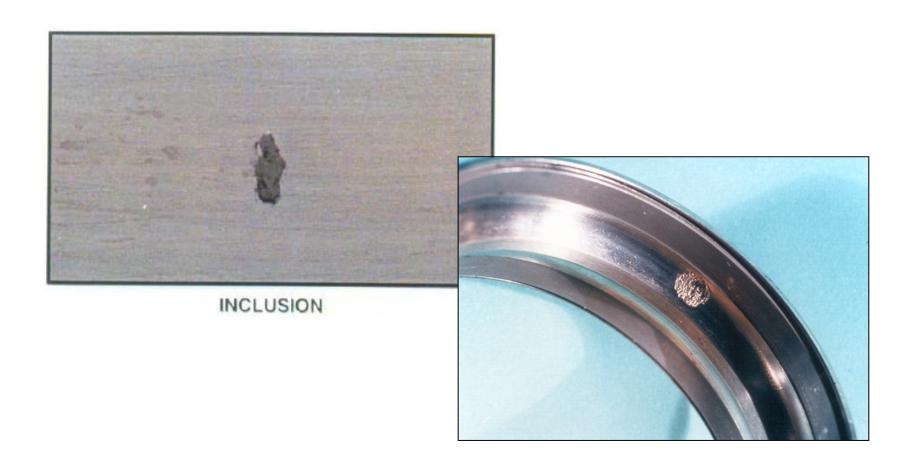
Material Fatigue: **Spalling**





Material Fatigue:

Inclusion Origin Spalling





Material Fatigue:

Point Surface Origin (PSO) Spalling



Spalling from debris or raised metal exceeding lubricant film thickness on a tapered roller bearing



Material Fatigue:

Geometric Stress Conc. (GSC) Spalling



Spalling from misalignment, deflections or heavy loading on a tapered roller bearing



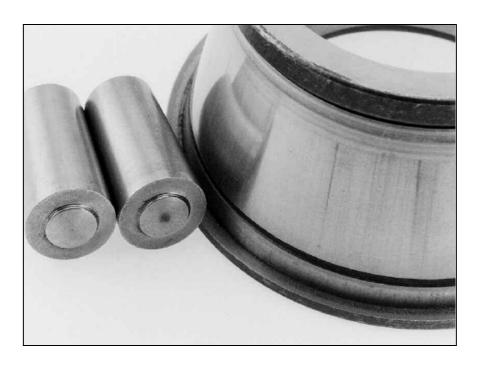
Bearing Damage Modes:

Wear or Other Damage

- Potential causes of wear or other damage are numerous:
 - Faulty mounting
 - Improper adjustment
 - Lack of lubrication
 - Contamination
 - Improper handling, storage, or transport
 - Improper maintenance
 - Exceeding machine limits
 - Environmental factors (temperature, atmosphere, etc.)
- Divide damage causes into (3) general categories:
 - Contamination
 - Inadequate Lubrication
 - Misuse



Contamination: Abrasive Wear



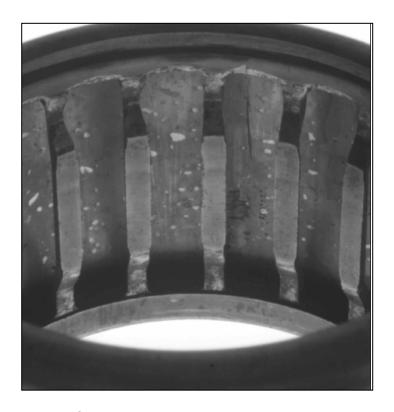
Tapered roller bearing abrasive wear



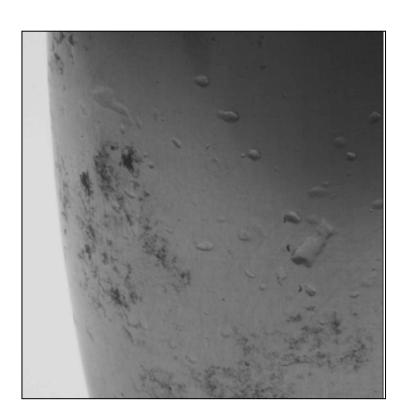
Spherical roller bearing fine particle contamination



Contamination: **Bruising**



Cylindrical roller bearing outer ring bruising



Contamination bruising from hard particles in spherical roller bearing



Contamination: **Denting**



Debris denting

Ball



Spherical roller

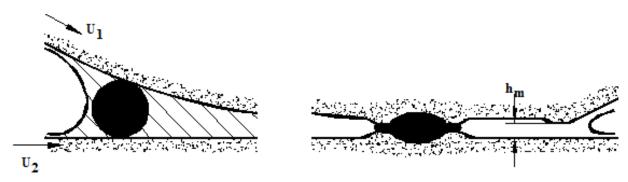


Tapered roller

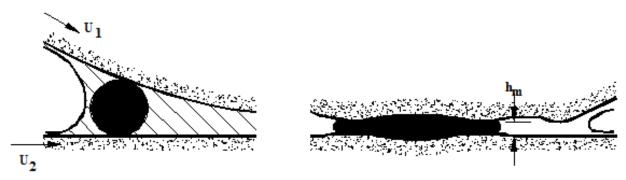


Contamination:

Soft vs. Hard Ductile Particles



Hard Ductile Particle



Soft Ductile Particle



Contamination:

Prevention of Particulate Damage

- Regular inspection of seals
- Ensure clean lubricant supply
- Use proper bearing removal, cleaning and replacement procedures
- Don't remove bearing from package until ready for mounting
- Ensure clean shop and tools
- Protect from dirt
- Regular maintenance or replacement of filtration elements. Do not bypass the filter.



Contamination: Etching / Corrosion



Etching and corrosion on cylindrical roller bearing inner ring



Advanced corrosion and pitting on the cone race and rollers



Contamination: Etching / Corrosion



Heavy water damage on a ball bearing inner ring and cage



A tapered roller bearing cup with corrosion on the race



Contamination: Etching / Corrosion Prevention

- Inspect and replace worn seals to avoid etching due to exposure to moisture
- Monitor moisture level in lubricant
- Ensure that bearings are stored in a dry area
 - Before storage, bearings should receive a coating of oil or other rust preventative
 - Wrap bearings in protective paper or covering
- After washing / cleaning, bearings should be thoroughly dried



Contamination: Fretting Corrosion



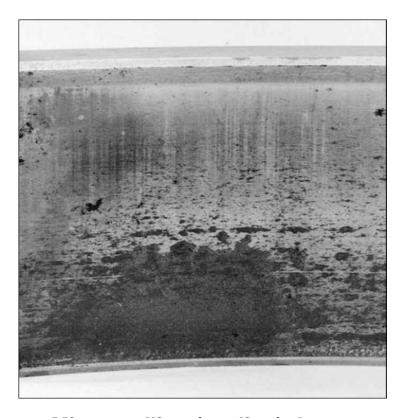


Inadequate Lubrication

- Any condition that allows metal-to-metal contact in a bearing can be regarded as "inadequate lubrication"
- Sources / Causes:
 - Lubricant starvation
 - Insufficient lubricant to sustain a film
 - Wrong kind of lubricant for the speed and load
 - Wrong grade of lubricant
 - Wrong type of lubricant system, such as the use of an oil level and splash system when operating conditions require a circulating system



Inadequate Lubrication: **Peeling**



Microspalling (peeling) due to thin film from high load/low RPM or high temperatures

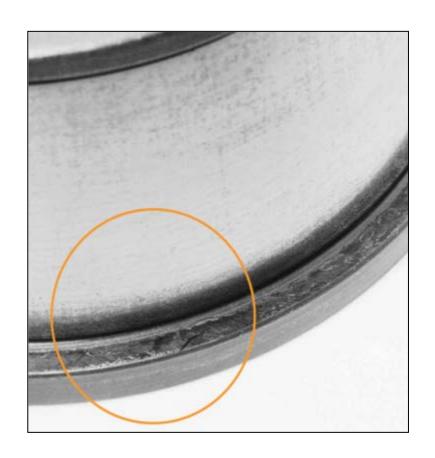


Inadequate Lubrication:

Rib – Roller End Scoring



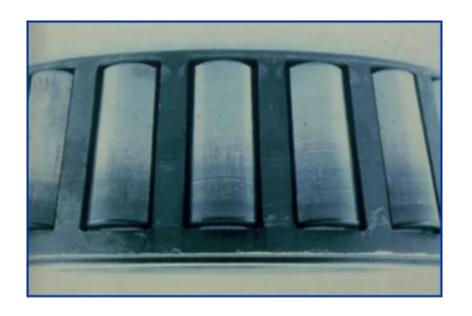
Heat damage on tapered rollers from metal-to-metal contact

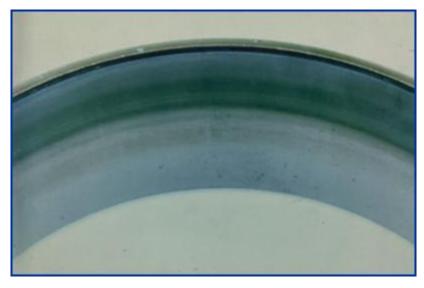


Scoring of tapered roller ends and rib face



Inadequate Lubrication: Heat Discoloration







Inadequate Lubrication: Smearing

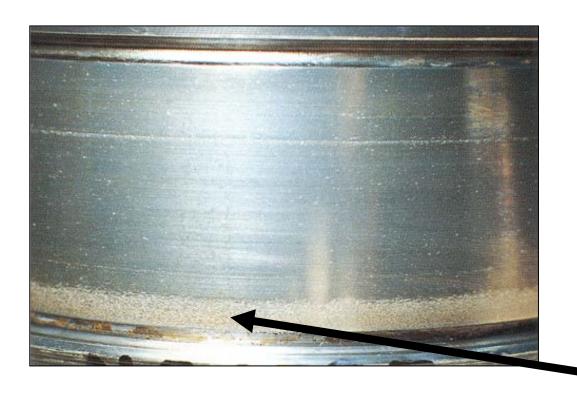


Thrust SRB Roller with Smearing Damage

Smear bands



Inadequate Lubrication: **Smearing**



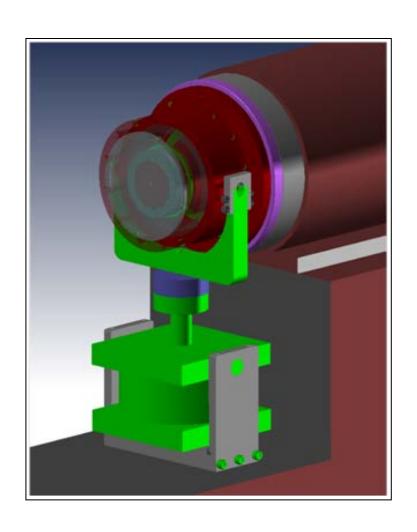
Smeared TRB Cone Raceway

Smearing

Goal – Produce smearing in full-scale CRB, and evaluate effectiveness of surface treatment options to mitigate it.



Test Equipment and Materials



Timken 4-S Test Rig

Rig Characteristic	Range or Description
Speed (rpm)	0 to 3600
Radial Load (kN)	0 to 44.5
Thrust Load (kN)	0 to 22.3
Temperature Sensing	Thermocouples for oil and test bearings
Spindle Torque	Inline torque meter
Cage Speed	Proximity sensor/tachometer
Vibration	Accelerometer



Test Equipment and Materials

- T-6411-A cylindrical roller bearing
 - NU-type.
 - OD = 290 mm, Bore = 160 mm,Width = 98.425 mm
- (4) test treatments, (3) bearings tested per treatment



Treatment ID	Treatment Description
Ground	Standard Ground Rings and Rollers
Honed / ES20	Honed Raceways, ES20 Roller Texturing
Honed / ES20 / Black Oxide	Honed Raceways, ES20 Roller Texturing, Black Oxide Treatment on both Rings and Rollers
Wear-Resistant	Honed Raceways, ES322 Texture and Coating on Rollers



Test Protocol

- It was not easy to achieve smearing!
- Attempted conditions include:
 - Steady state load and speed conditions for short and long test durations
 - Monotonic load level step-down at constant speed
 - Oscillating load level between a constant "high" level and successively lower step levels at constant speed
 - Oscillating load level between a constant "low" level and successively higher step levels at constant speed
 - Stepping the load level above and below a constant "medium" level at constant speed
 - Fixing various constant load levels and dropping the speed to a low level and then rapidly accelerating to a higher level
 - Various oil type, temperature, and starvation conditions
 - etc...



Test Protocol

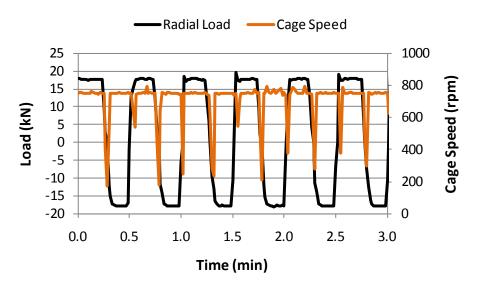
- A constant speed test with a two-stage radial load profile worked.
 - 1st load stage: square wave, alternating load direction between 12 & 6 o'clock.
 - 2nd load stage: nominal "zero" load condition (small load to offset shaft weight).

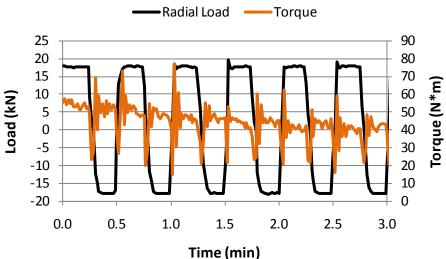
Test Parameter	Value
Load (kN) (as a function of time in min)	$P(t) = \begin{cases} 17.8(-1)^{\lfloor 4t \rfloor}, & \text{if } 0 \le t \le 40\\ 0.7, & \text{if } 40 < t \le 100 \end{cases}$
Speed (rpm)	1800
Oil Flow Rate (mL/min)	47.3
Oil Inlet Temp	Not Controlled – Lab Temp
Oil Type	SAE 20, Polyalphaolefin Synthetic with no EP/AW Additives
Total Test Duration (min)	100

^{* 17.8} kN is ~1.5% C1 rating for bearing



Full-Scale CRB Smearing Test Program: **Test Results**

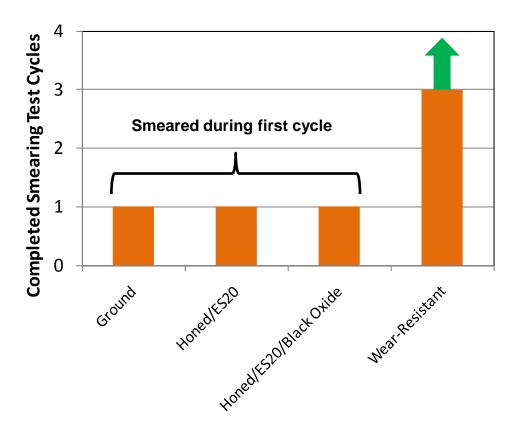




- Smearing achieved by creating high rollerraceway sliding conditions via load direction reversal.
- First (3) mins of a representative test shown at left:
 - Significant drop in cage speed during load disengagement and subsequent cage/roller acceleration on reengagement.
 - Accompanying torque instability during load direction change.



Test Results



Each bar represents (3) replicate tests from which no variation in result from test to test was observed. That is, all WRB tests were suspended after 3 test cycles with no smearing. All standard tests smeared after 1 test cycle, etc.



Post-Test Bearing Analysis



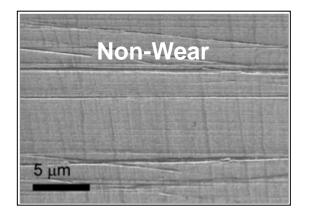


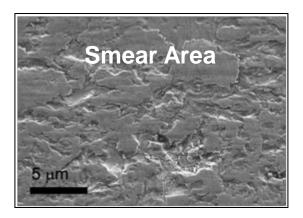




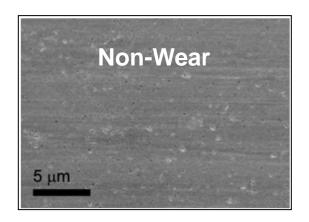


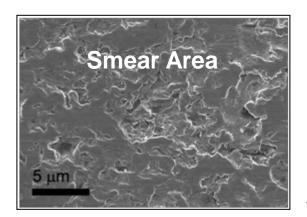
Post-Test Bearing Analysis





Honed/ES20



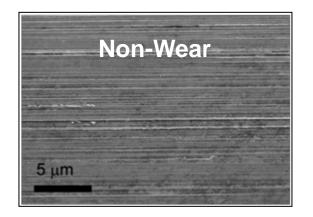


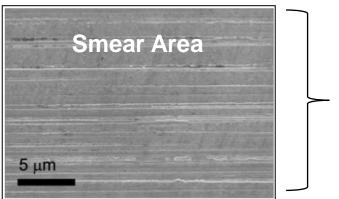
Honed/ES20/Black Oxide





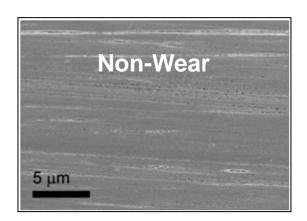
Post-Test Bearing Analysis





Mild Plastic Deformation

Ground



No smear area

Wear-Resistant

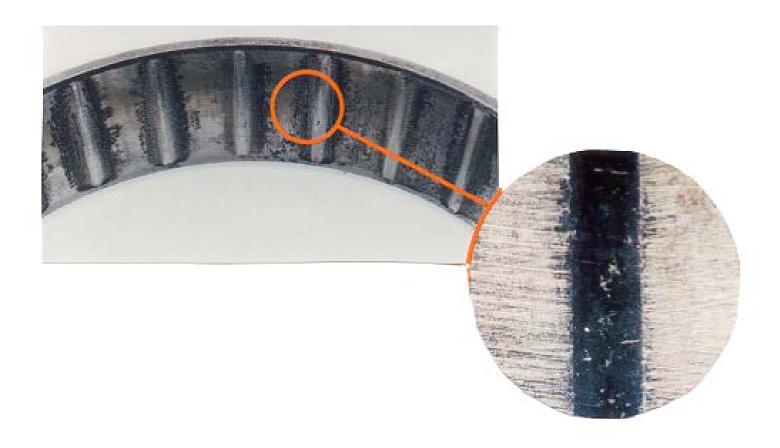


Post-Test Bearing Analysis

- Smearing damage was achieved in full-scale CRB using a two-part test with a period of repetitive load direction reversals (load ~1.5% of the C1 dynamic load rating) followed by steady operation at a nominal zero-load condition.
- Wear-Resistant bearings featuring special roller coatings were the only treatment that prevented smearing in these tests.
- Black oxide treatment did not provide additional smearing protection over the Honed/ES20 case that had similar raceway and roller body roughness in these tests.
- Surface finish and roughness specifications must be carefully considered in applications that are susceptible to smearing.



Inadequate Lubrication: False Brinelling





Inadequate Lubrication: **Prevention**

- Ensure that an appropriate amount of the correct type and grade of lubricant is present
- In environments where lubricant may be washed out, select a sealed bearing
- Ensure that the correct lubricant delivery system is used
- Proper grease pack/distribution
- Ensure flow starts before rotation or operation
- Ensure proper function of lube system: proper flow rates, proper settings and maintenance of metering devices
- Ensure proper temperature in oil sump or inlet



Excessive Preload or Overload



Overloading on a cylindrical roller bearing caused roller surfaces to fracture



Overloading resulted in severe fatigue spalling on the tapered rollers



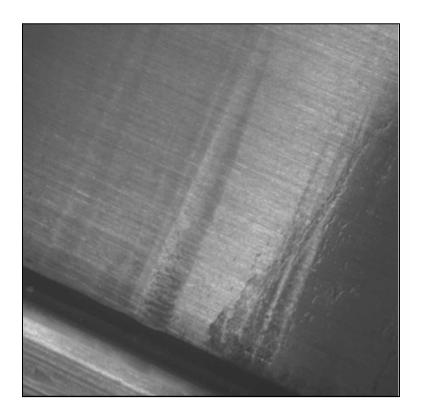
Excessive Preload or Overload



Overloading and low speed caused insufficient lubricant film



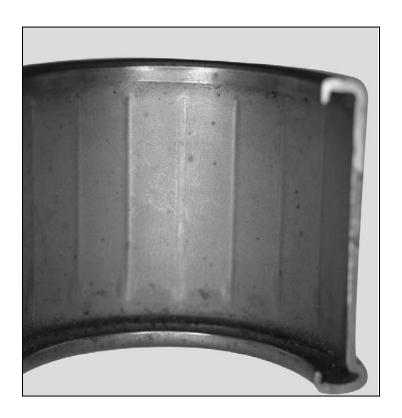
True Brinelling



Spherical roller bearing inner ring showing roller impact damage from shock loading



True Brinelling

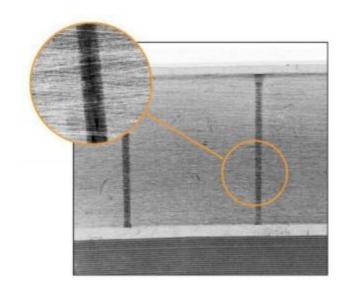


Needle roller bearing outer ring race with rollerspaced indents from impact during installation

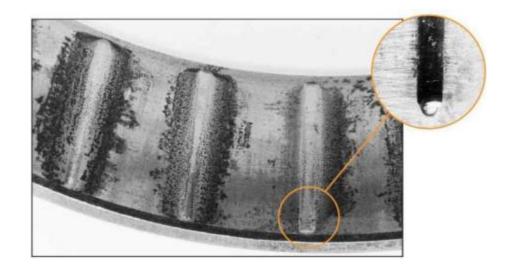


True vs. False Brinelling

 False brinelling wears away the surface texture, while the original surface texture remains in the depression of a true brinell



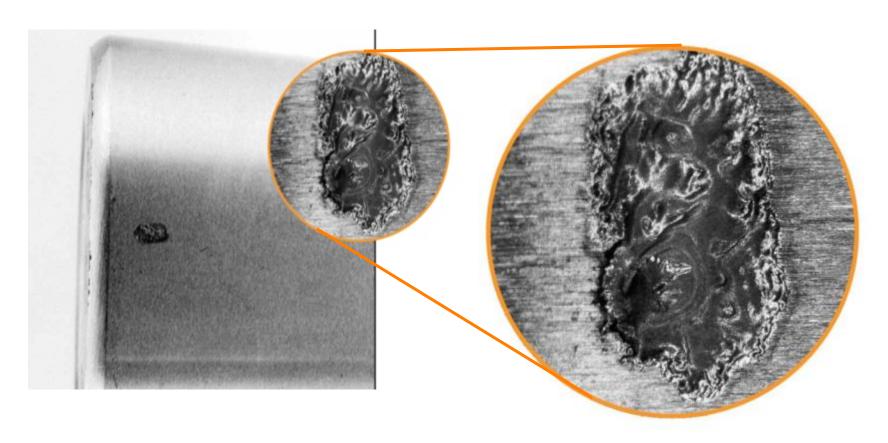
True Brinelling



False Brinelling



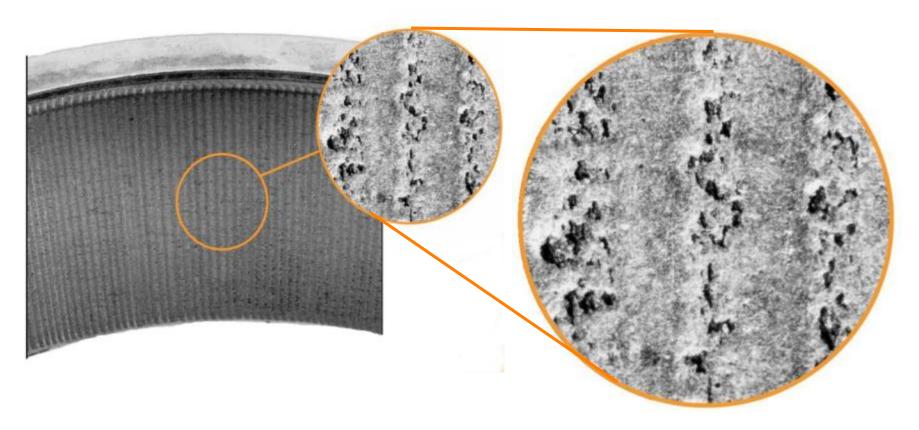
Burns from Electric Current



Pitting / small burns created by arcs from improper electric grounding in stationary bearing



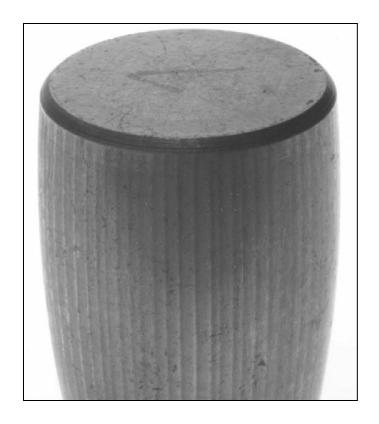
Burns from Electric Current



Fluting (small axial burns) caused by electric current passing through rotating bearing



Burns from Electric Current



Roller with fluting caused by welding performed on machine while bearings were rotating



Keys To Optimal Bearing Performance

Proper:

- Selection/Specification
- Handling
- Installation
- Lubrication
- Sealing
- Cleaning

Minimize Contamination, Inadequate Lubrication, and Misuse!



What are White Etch Areas?

- Microstructural Alterations: Phase transformations that occur during service due to high application stresses and/or long service lives.
- The location of nucleation sites for these phase transformations can be found to be either:
 - Random (within a depth interval consistent with high applied stresses – e.g., 0.005"-0.023")
 - Dark etch regions
 - White etch areas
 - Specific (at lower strength areas or stress risers within the original microstructure or steel)
 - White bands
 - Butterfly



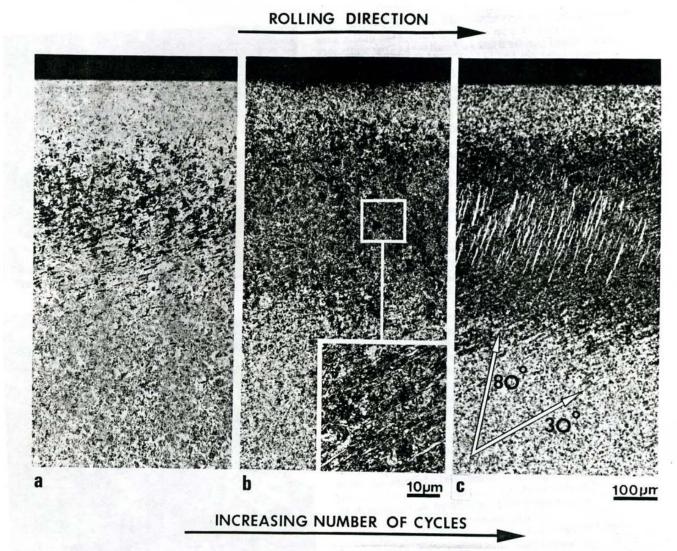
Microstructural Alterations - Terminology

- Dark Etching Areas
 - Dark Tint
 - Dark Line
 - Dark Etching Regions (DER)
 - Dark Needles
 - Dark Etching Bands
- White Bands
 - 80 or 30 Degree Bands
 - White Etch Areas (WEA)
 - White Etching Alterations (WEA)
 - Light Etching Areas
 - Light Etching Region
 - Bright Etching Regions (BER)
 - High/Low Angle Bands
 - Steep/Flat White Band

- Butterfly
 - Stress Butterfly
 - White Etch Areas
- White Etch Cracking
 - White Etch Areas (WEA)
 - Brittle Flaking
 - White Structure Flaking
 - White Band
 - Bright Etched Regions
 - irWEA
 - irregular white etch areas
 - Inner ring white etch areas
 - Axial Cracking
 - Radial Cracking



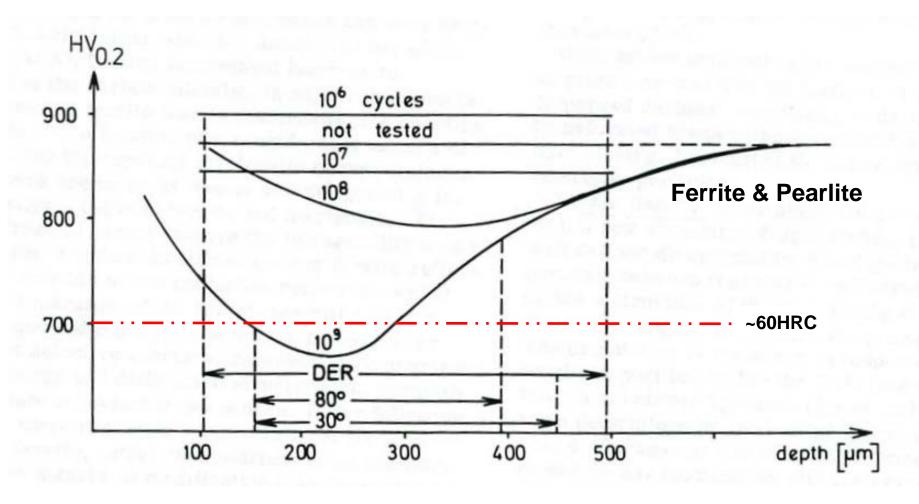
Dark Etching Areas & White Bands



Accumulation of subsurface damage with increasing cycles.



Dark Etching Areas – Hardness Changes





Butterfly – Morphology & Orientation



Butterfly – Micro Hardness

- SAE 52100
- Knoop Hardness
- Used 25 gram load
- 3% Nital Etch
- Originally 800X
- Nomarski Polarized Lighting

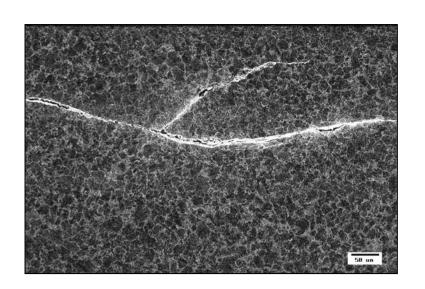
- Matrix = 825 KHN = HRC 64
- Butterfly = 1780 KHN>> HRC 70

Source: Torrington Met Lab Archive

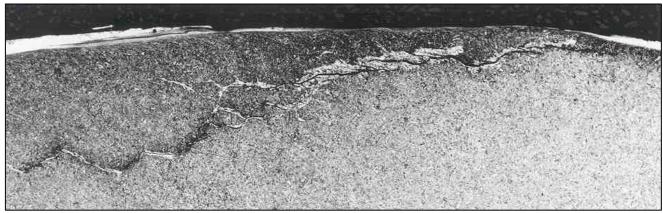




White Etch Cracking

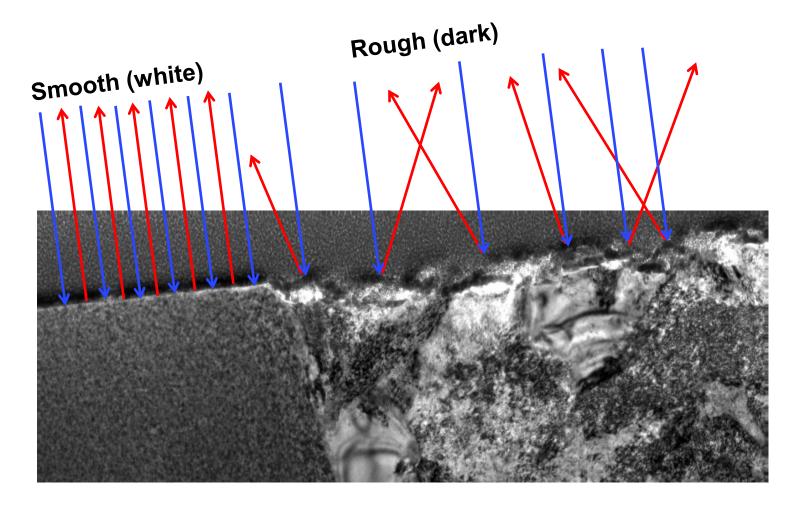






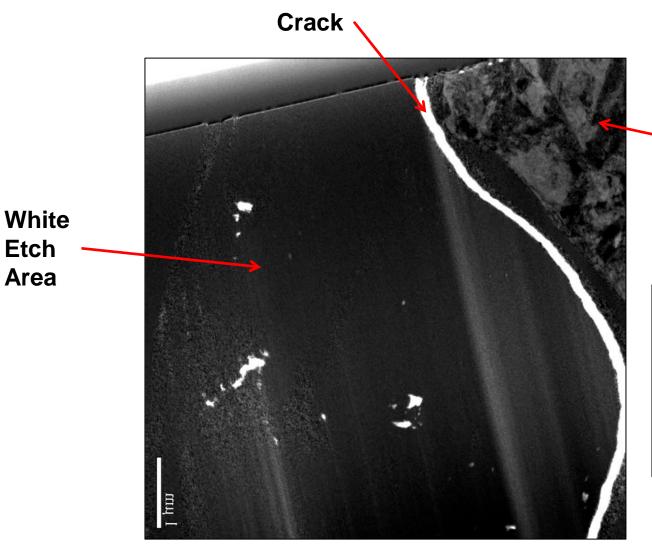


White Etch Areas - TEM





White Etch Areas - TEM



Original Microstructure





White Etch Area Take-Aways

- Investigations are underway to better understand WEA network microstructural alterations and their causes.
- Current understanding is that WEA are linked to brittle flaking and possibly axial cracking as well.
- Literature and analogies between WEA networks and stress butterflies/DER-WBs point toward a mechanical root cause, likely involving high stress and slip conditions.





Summary

- It is usually easy to see bearing damage, but often difficult to determine the cause.
- In many cases the bearing damage may be due to a combination of causes.
- Requires complete investigation of mounting, installation and related parts.
- Smearing was achieved with full-scale CRB in the lab by oscillating the load zone direction, and only Wear-Resistant bearings were able to survive without smearing under those conditions.
- A study of WEA microstructural alterations is underway.



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- G. Doll, P. Shiller from the Timken Engineered Surfaces Laboratory at the Univ. of Akron.

Questions?



Where You Turn